foil elements were parallel and 1.2 cm apart. Both foils were monitored in the same way but no external current was sent through the passive foil. The passive foils exhibited a signal of about 2 millivolts on shock arrival. This compares to more than 70 millivolts from active foils carrying 150 amperes of external current. The 2-millivolt signal is attributed to inductive coupling. The passive foil was coupled to the high current in the other foil via eddy currents in the moving metal impactor. At any rate, we can conclude that the signal observed on shock arrival at the foil in ensuing experiments is due to current in that foil. By using Ohm's law we can with confidence attribute the signal to the resistance change in the foil.

Table II presents the results of shot data analysis according to Fig. 4. The experimental resistance ratio (column 1) $R / R_{o}=E / E_{o}$ is converted to resistivity (column 2) by

$$
\begin{equation*}
\frac{\rho}{\rho_{0}}=\frac{R}{R_{0}} \frac{V}{V_{0}} \tag{Sec.II.A.5}
\end{equation*}
$$

The shock temperature rise $\Delta \mathrm{T}_{\mathrm{H}}$ in column 3 is calculated as described in Sec. III.E.I, and columns 4 and 5 give the resistivity change due to temperature rise and isothermal shock resistivity calculated from the results of Sec. III.A.4. The last column gives the resistivity deviation between isothermal shock resistivity and calculated hydrostatic resistivity (Sec. IV.D).

TABLE II. Results of data analysis.

| Shot No. | Resistance Ratio $\frac{R}{R_{0}}$ | $\begin{aligned} & \begin{array}{l} \text { Resistivity } \\ \text { Ratio } \end{array} \\ & \left(\frac{\rho}{\rho_{0}}\right)_{\text {Expt. }} \end{aligned}$ | Temperature Rise $\Delta \mathrm{T}_{\mathrm{H}}\left({ }^{\circ} \mathrm{C}\right)$ | Thermal Resistivity Change $\frac{\Delta \rho_{T}}{\rho_{0}}$ | Isothermal Resistivity Ratio $\frac{F\left(V, T_{0}\right)}{\rho\left(V_{0}, T_{0}\right)}$ | Defect Resistivity $\frac{\Delta \rho_{D}}{\rho_{0}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 72-065 | 1.051 | 0.992 | $\sim 51$ | 0.16 | 0.83 | -- |
| 72-068 | 1.170 | 1.086 | $\sim 74$ | 0.21 | 0.88 | -- |
| 72-069 | 1.073 | 0.995 | 71.6 | 0.190 | 0.797 | 0.072 |
| 73-009 | 1.049 | 0.982 | 58.6 | 0.160 | 0.813 | 0.058 |
| 73-010 | 1.058 | 0.990 | 58.9 | 0.161 | 0.820 | 0.066 |
| 73-011 | 1.022 | 0.974 | 39.3 | 0.113 | 0.853 | 0.039 |
| 73-013 | 1.000 | 0.977 | 17.6 | 0.052 | 0.917 | 0.013 |
| 73-027 | 1.120 | 1.031 | 81.8 | 0.211 | 0.810 | 0.106 |
| 73-028 | 1.035 | 0.995 | 31.3 | 0.094 | 0.895 | 0.052 |
| 73-029 | 1.032 | 0.990 | 33.4 | 0.099 | 0.884 | 0.049 |
| 73-034 | 1.087 | 1.014 | 63.1 | 0.170 | 0.834 | 0.090 |
| 73-036 | 1.122 | 1.050 | 59.4 | 0.162 | 0.879 | 0.126 |
| 73-040 | 1.037 | 0.987 | 40.8 | 0.117 | 0.862 | 0.053 |
| 73-044 | 1.111 | 1.039 | 59.9 | 0.170 | 0.870 | 0.120 |
| 73-047 | $1.149 \pm .013$ | 1.071 | 63.7 | 0.178 | 0.894 | 0.152 |
| 73-050 | 1.185 | 1.09 | 82.5 | 0.220 | 0.872 | 0.170 |
| 73-059 | 1.139 | 1.045 | 84.0 | 0.219 | 0.821 | 0.122 |

